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1 **Emissions down the drain: Balancing life cycle energy and**
2 **greenhouse gas savings with resource use for heat recovery from**
3 **kitchen drains**

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10
11 **Abstract**

12 Although the food service sector is a major user of water, the potential for heat recovery from
13 commercial kitchens' drain water remains largely unexplored. For the first time, we compare
14 the life cycle environmental burdens of producing and installing a heat recovery system with
15 the environmental credits arising from energy savings for a restaurant case study, and for the
16 entire UK food service sector. Life Cycle Assessment was applied to determine the impacts of
17 heat recovery systems made from different materials and comprising a heat exchanger in the
18 shape of a concentric double-walled pipe, pipework and fittings. The design option with the
19 smallest environmental footprint combined a heat exchanger made out of polypropylene-
20 graphite (PP-GR) with polyethylene pipework, exhibiting 80-99% less environmental impact
21 compared with components made out of (35% recycled) copper. Contrasting the
22 environmental impacts of two heat recovery set-ups with energy savings shows that a PP-GR
23 based system pays back all seven assessed environmental impacts within two years, while
24 payback times for the copper-based system vary depending on the replaced energy source,
25 and can exceed the 10 year operational lifetime of the system. When looking at typical flow-
26 rates in UK food outlets, net environmental savings can be realised across all analysed impact
27 categories above a threshold water consumption of 555 L/day, using current technology.
28 Extrapolation to the UK food service sector indicates annual greenhouse gas emission
29 mitigation potential of about 500 Gg CO₂ equivalent.

30
31 **Keywords**

32 Environmental impact assessment, wastewater heat recovery, energy savings, eco-design,
33 climate change mitigation, recycling

34
35 **1 Introduction**

36 In the UK, nearly half of the water consumption of the wider food and drink sector occurs in
37 the hospitality and food service sub-sector, with an estimated 143 million m³ water used in
38 2010 for the preparation of meals in commercial and similarly used kitchens (Bromley-
39 Challenor et al., 2013). Spriet and McNabola (2019a) determined a total wastewater heat
40 recovery potential for the UK food service sector of 1.4 TWh/year, and a financially viable

41 potential of 1.24 TWh/year. The recovered heat is available for direct reuse for pre-heating the
42 cold water supply and can hence directly contribute to the decarbonisation of hot water use.
43 Heating water accounts for a considerable amount of energy consumption across industrial
44 and non-industrial sectors. It is estimated that up to about 90% of the energy requirements
45 and related greenhouse gas (GHG) emissions from the domestic water cycle in industrialised
46 countries derive from heating water (Arpke and Hutzler, 2008; DEFRA, 2008; Fagan et al.,
47 2010; Gerbens-Leenes, 2016; Nair et al., 2014; Siddiqi and Fletcher, 2015). Sanders and
48 Webber (2012) looked into the energy consumption for water use of all sectors in the US, and
49 found that heating for hot water and steam generation dominated water-related energy
50 consumption not only in the residential, but also the commercial and industrial sector.
51 Altogether, 47% of the US primary energy consumption in 2010 was due to water and steam
52 applications (Sanders and Webber, 2012).

53 While heat recovery from wastewater has been intensively studied and applied in the
54 residential sector, this is not the case for the food service sector, although the same appliances
55 can be used. The necessary equipment for heat recovery from drain water on a small-scale
56 includes market-ready low-tech options such as in-line, pipe shaped heat exchangers (Ip et
57 al., 2018; McNabola and Shields, 2013; Schuitema et al., 2005; van der Hoek, 2011). They
58 have been predominantly studied and installed for use in households or similar domestic
59 settings for shower or mixed drain water (Ip et al., 2018; McNabola and Shields, 2013;
60 Schuitema et al., 2005; Słyś and Kordana, 2014; Wong et al., 2010). However, they could also
61 be potentially used with other wastewater types.

62 A bonus of heat recovery from commercial kitchens' drain water is a higher daily water use
63 compared to an average household, which for the UK lies in the range of 360 to 12,500 L/day
64 (Spriet and McNabola, 2019a), versus to 349 L/day in homes (EST, 2013). The heat recovery
65 figures by Spriet and McNabola (2019a) equate to an average yearly saving of about
66 5400 kWh per food outlet. Installation of comparable heat recovery systems with showers
67 have been reported to save 127-1880 kWh/year per six showers in a sports facility (Ip et al.,
68 2018), and 130-508 kWh/year per one shower in a residential building (Wong et al., 2010).
69 The amount of heat energy recovered during the lifetime of the heat recovery system plays an
70 important role not only for financial payback, but also environmental payback for the
71 installation.

72 As with all manufactured products, heat recovery devices carry environmental burdens
73 through their manufacture, installation works, operation and disposal. Significant burdens from
74 manufacture are especially associated with metals such as copper, which is frequently used
75 for plumbing equipment and a preferred material for heat exchangers because of excellent
76 heat conducting properties. It is known that production of copper components generates larger
77 environmental burdens compared to steel (Prek, 2004) or plastic (Asadi et al., 2016; Franklin
78 Associates, 2011), with regard to GHG emissions (Franklin Associates, 2011), human health
79 and eutrophication impacts (Asadi et al., 2016). Hence, to justify the application of heat
80 recovery devices on resource efficiency and wider environmental grounds, the impacts
81 generated during their life cycle have to be considered. However, there is a lack of studies
82 evaluating in-line heat recovery devices for small-scale applications, and providing the
83 complete picture of environmental impacts through full Life Cycle Assessment (LCA). The
84 most comprehensive related study was published by Ip et al. (2018), who conducted an
85 environmental and economic assessment of an in-line heat exchanger from copper recovering
86 heat from shower drains in a university sports facility. Whilst their LCA study comprised all
87 steps, from cradle to grave (manufacture, use and end-of-life) of the heat exchanger, it only
88 considered the Global Warming Potential (GWP) burden; i.e. GHG emissions. Other impact
89 categories such as resource depletion with material component manufacture were not

90 included. The study also did not consider the need for additional pipework or fittings that can
91 be necessary to connect the heat recovery device to a boiler, especially when retrofitting an
92 existing plumbing system.

93 Here, we apply LCA methodology to determine for the first time the environmental burdens
94 across seven impact categories arising from the manufacture and retrofit installation of a full
95 drain water heat recovery system suitable for use with kitchen drain water. Besides the
96 essential heat exchanger, the system consists of the pipework required for connecting the
97 heat exchanger to a boiler and cold water supply, of insulation and fittings. Due to important
98 potential environmental trade-offs associated with copper highlighted in aforementioned
99 studies, we explore the use of recycled copper and of a polymer based material as alternative,
100 namely polypropylene-graphite (PP-GR). For pipework, different materials (copper, steel,
101 polyethylene) and different lengths are considered, in order to represent different site-
102 dependent conditions.

103 As the amount of recoverable heat and the benefits derived from avoided water heating
104 significantly influence the environmental sustainability of heat recovery systems, LCA results
105 are compared to energy savings from different sizes of kitchens used for different purposes:
106 the comparison includes savings from a case study restaurant and from commercial kitchens
107 across the UK food service sector. Eventually, extrapolation of the findings to the UK food
108 service sector determines the potential savings on a national level.

109 **2 Materials and methods**

110 **2.1 Goal and Scope**

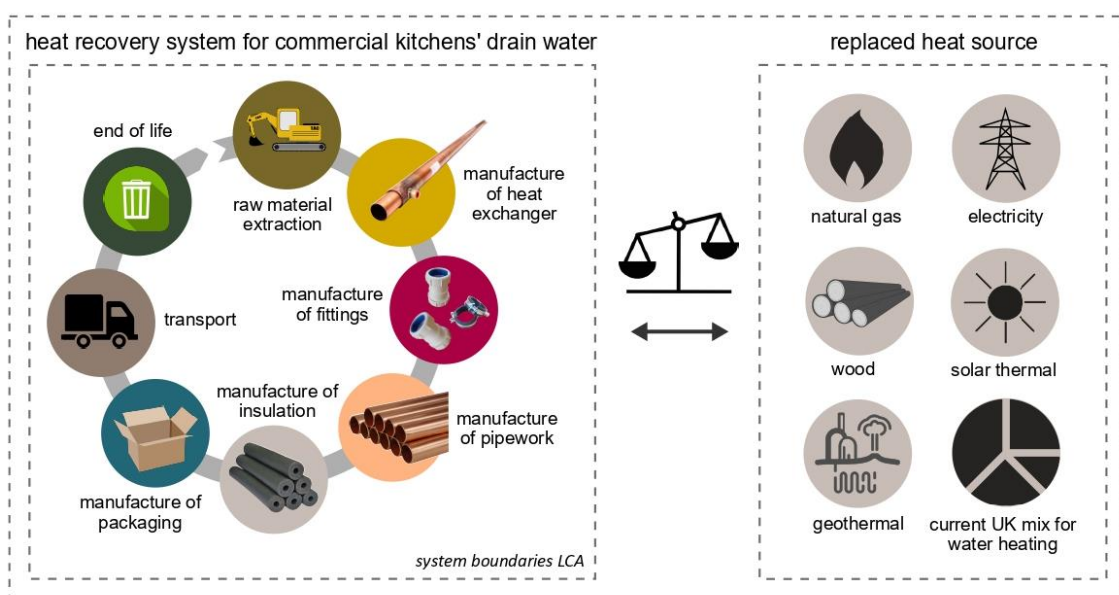
111 The objective of this study is to provide a comprehensive picture of the environmental burdens
112 of a heat recovery system retrofitted to a commercial kitchen, to identify the steps in the life
113 cycle contributing most to these environmental burdens and to explore the role for alternative
114 materials to mitigate “hotspots” of environmental impacts, and inform eco-design. The LCA
115 approach has been chosen for this purpose, following the guidelines of ISO 14040 (ISO,
116 2006). An LCA accounts for resource use and emissions arising during the life of a product or
117 service, starting with resource extraction and mining, and ending with its disposal or alternative
118 end-of-life (EoL) management. In the case of the copper pipe, it includes for instance the
119 mining of the copper ore, through processing of the copper such as melting and extrusion, to
120 recycling into new copper products.

121 Environmental impacts are classified into different impact categories, with Global Warming
122 Potential (GWP) caused by GHG emissions being the most prominent one. We furthermore
123 chose the following environmental impact categories from the set of categories and
124 characterisation methods recommended at midpoint level by the International Reference Life
125 Cycle Data System (ILCD) (EC JRC 2011): Human Toxicity Potential (HTP) and Freshwater
126 Ecotoxicity Potential (FEToxP), as these impacts are associated to mining activities such as
127 copper mining; Mineral, fossil & renewable Resource Depletion Potential (RDP), as nearly all
128 parts of the heat recovery systems assessed are made from finite materials and changes are
129 expected with different recycled material input rates; Freshwater Eutrophication Potential
130 (FEP), Acidification Potential (AP), and Photochemical Ozone Formation Potential (POFP), as
131 they are connected to a variety of industrial processes such as mining, fossil fuel combustion
132 in heat and electricity generation as well as transport. Eutrophication is furthermore associated
133 with energy generation from biomass. HTP is presented as sum of both the cancer and non-
134 cancer toxicity potential. Normalised scores have been obtained in SimaPro, with
135 normalisation factors based on Benini et al. (2014).

136 The life cycles of the heat recovery systems are modelled with the software SimaPro (release
 137 9.0) (PRé Sustainability, 2018) and using the Ecoinvent (2018) version 3.5 database for the
 138 life cycle inventory for the majority of processes (see Supplementary Material S1 for additional
 139 databases used).

140 2.2 System boundaries

141 The LCAs include all stages from cradle-to-grave, i.e. from the extraction of the raw materials
 142 incorporated in the processes chosen from the database until the end of life of the products
 143 (Figure 1). No environmental burdens are considered to arise during the use phase, as the
 144 device itself is passive and not expected to create any emissions. Maintenance (i.e. cleaning)
 145 intervals are unknown, and cleaning burdens are estimated to be minor compared to overall
 146 lifecycle burdens. Packaging and transport are included. Transport is part of both the
 147 foreground system and the background system through choice of appropriate processes from
 148 the databases (Supplementary Material S1).



149
 150 *Figure 1: System boundaries of the LCAs on the heat recovery system (left, shown for the copper system) and*
 151 *extended boundaries for evaluating the savings potential through the replacement of heat energy sources.*

152 2.3 Description of the system and inventory

153 2.3.1 Overview

154 The core part of the heat recovery system is the heat exchanger designed as a concentric
 155 double-walled pipe which replaces a part of the wastewater pipe. The warm wastewater flows
 156 through the inner pipe, while the cold incoming water flows in the opposite direction through
 157 the outer pipe (counter flow principle, Supplementary Material S2). For a fully functional heat
 158 exchanger and maximum heat recovery, the warm drain water has to form a falling film along
 159 the wall of the inner pipe (Manouchehri et al., 2015). This is enabled through a vertical
 160 installation (Manouchehri et al., 2015). The heat exchanger is connected to the existing
 161 pipework via plastic fittings (bottom and top connectors) with joint rings, one fitting each end
 162 of the pipe (BPD Ltd., 2019a). Screws and brackets made from steel and rubber fix the heat
 163 exchanger at the wall (BPD Ltd., 2019a).

164 The pre-heated incoming water is led from the heat exchanger to the conventional heating
165 system, usually a boiler, for further heating. Depending on the layout of the existing plumbing
166 in a building, the heat exchanger cannot be placed in close vicinity to the boiler or the incoming
167 cold water pipe and additional pipework can be required to cross the distance. To minimise
168 heat loss, the pipework is considered to be insulated with a layer of synthetic rubber.

169 An overview of the inventory is provided in the Supplementary Material S1.

170 **2.3.2 Manufacture of the copper heat exchanger**

171 Description: The heat exchanger considered refers to a model which is 1.68 m long, has an
172 inner diameter of 48 mm and weighs 6.1 kg (Q-Blue b.v., 2018). The capacity for the drain
173 water flow is 50 L/min, and the maximum clean water flow is 12 L/min. The clean water void
174 between the inner and outer cylinder has a volume of 0.39 L.

175 Modelling: Starting with primary or recycled copper, the production of a semi-finished copper
176 tube continues with the following steps: melting, casting, extrusion, drawing and finishing steps
177 from the raw pipe to the final heat exchanger (Tikana et al., 2005). As the processes of melting
178 and casting are already included in an Ecoinvent database process for primary copper
179 production, they are only modelled separately for the recycled copper. For melting the
180 secondary copper, we assume the electricity input for an induction furnace, which is the type
181 of furnace predominantly used in the copper industry (CDA Inc., 2019). The energy
182 requirement for melting of copper in an induction furnace is calculated according to basic
183 physical principles and a plant efficiency of 70% (Dötsch, 2017) (Supplementary Material S3).

184 As primary copper production is a resource- and energy-intensive process, responsible for
185 considerable emissions during mining, ore refining and further processing (Althaus and
186 Classen, 2005; Castro Molinare, 2014), adequate assumptions for the share of recycled
187 copper in the heat exchanger are necessary for a realistic picture of its environmental impacts.
188 Two types of recycled or secondary copper can be distinguished: recycled scrap, which
189 originates from low grade copper scrap and which has to be refined electrolytically before
190 reuse; and clean scrap, which can be directly re-melted.

191 Studies from Ciacci et al (2017) and Glöser et al (2013) estimated an average 35% recycling
192 input rate for all types of copper products in Europe and globally, of which 63% is clean scrap.
193 Another study, commissioned by the copper industry and claiming to rely on primary industry
194 data, assumes a share of around 70% of recycled copper as input for the production of
195 European copper pipes, of which about 90% comes from clean scrap (Tikana et al., 2005).

196 **2.3.3 Manufacture of the PP-GR heat exchanger**

197 PP-GR has been chosen in this study as a potential substitute for copper in a wastewater heat
198 exchanger for several reasons. It exhibits a greater fouling and corrosion resistance compared
199 to metals, which is important when conveying media heavily loaded with organic material, such
200 as kitchen wastewater (Chen et al., 2016; Hussain et al., 2017, Glade et al., 2018). As PP-GR
201 has been tested and designed for use in highly corrosive environments such as desalination
202 plants and with higher temperatures than those of kitchen wastewater, we expect the material
203 to be appropriate to handle wastewater (Glade et al., 2018; Technoform, 2014). From an
204 environmental perspective, a great advantage is the smaller amount of energy required for
205 forming polymers, compared with metals.

206 Description: There is no commercially available heat exchanger made from PP-GR to date
207 that is equivalent to the copper model evaluated here. Material requirements are therefore
208 calculated for a hypothetical heat exchanger with the same length and volume for the water

209 leading parts in order to compare the amount of recovered heat. As PP-GR has a considerably
210 lower density than copper, at 1.56 g/cm³, only 1.02 kg material is required. The PP-GR
211 composite is made of polypropylene as a matrix with graphite as filler, imparting a thermal
212 conductivity comparable to that of stainless steel (Glade et al., 2018). PP-GR contains 72 wt%
213 graphite, equalling 50 vol% (Glade et al., 2018).

214 Modelling: Information on the material composition and properties were attained from a
215 manufacturer (Technoform, 2014) as well as from a study on its mechanical, chemical and
216 thermal properties (Glade et al., 2018). Virgin polypropylene and battery grade graphite are
217 considered as the inputs for the PP-GR pipe. Battery grade graphite production requires
218 energy intensive steps, comes with a higher environmental burden than that for graphical
219 paper and is therefore selected as a conservative proxy, so as not to underestimate
220 environmental burden (Olson et al., 2016). The tube is produced through an extrusion process.

221 In contrast to the copper device, no field data are available for the heat recovery potential of
222 the PP-GR heat exchanger in the discussed application. But given a heat transfer coefficient
223 of the PP-GR tube of 2523 W/(m²*K) (Technoform, 2014), we can determine an effectiveness
224 of 60.5%, close to that of the copper heat exchanger of 58% on average, according to the
225 manufacturer (Q-Blue b.v. 2018, Spriet and McNabola, 2019a) (Supplementary Material S4).
226 Heat recovery potential by the PP-GR device is therefore conservatively assumed to be equal
227 to that for copper.

228 **2.3.4 Pipework, insulation, fittings and packaging**

229 Pipework required to retrofit the heat exchanger within the existing plumbing network is also
230 accounted for. The outer diameter of this pipework is 28 mm (DN25), and we consider three
231 lengths to represent different retrofit situations: 1 m, 10 m (the length required in the case
232 study), and 30 m. Copper, steel and polyethylene are compared as pipe materials. Information
233 to model the pipework was retrieved from pipe manufacturers for copper (German Pipe, 2019),
234 polyethylene (Pipelife UK, 2019) and stainless steel (Geberit Sales Ltd, 2019). The insulation
235 is modelled using a pipe insulation module from Ecoinvent, which refers to insulation made
236 from the synthetic rubber ethylene propylene diene methylene (EPDM). Information on the
237 quantities and types of material of the fittings were derived from a manufacturer and a supplier
238 (BPD Ltd., 2019b; Q-Blue b.v., 2018). The weights of the parts and packaging were determined
239 directly by the authors.

240 **2.3.5 Transport**

241 The city of Birmingham has been chosen as a representative, central location within the UK
242 for installation of the heat recovery system. The copper heat exchanger and the fittings are
243 considered to be shipped from the Netherlands to the UK by lorry, unless more specific
244 information has been provided by a supplier for particular fittings (Livingston, 2018). Two parts
245 of the top connector are produced in Poland, and the third part is made in the UK along with
246 the entire bottom connector. The PP-GR heat exchanger in contrast is shipped from the
247 production site in Kassel, Germany. The pipework and insulation is assumed to originate from
248 Germany. The transport from the site of use to a recycling facility or landfill site is considered
249 using a generic distance of 100 km.

250 **2.3.6 End-of-Life**

251 The LCAs regard recycling for parts where a recycling infrastructure exists in the UK, and
252 landfill where recycling is unlikely. Different methodologies exist to allocate burdens for
253 recyclable materials in LCA (Ekvall and Tillman, 1997; Johnson et al., 2013). Here, we opt for
254 the cut-off or recycled content approach (Johnson et al., 2013) and hence do not account for

emissions and benefits from recycling in the EoL stage, as the recycling benefits and burdens in the manufacturing stage are already taken into account, where applicable. For copper, we assume recycling of 80%, which is the EoL processing rate for European plumbing equipment as determined by Ruhrberg et al. (2006). The remaining copper is considered to go to landfill. Bottom and top connectors are recycled completely, as their size allows for municipal waste management for hard plastics. Brackets and screws are assumed to go to landfill, as it is unlikely that the user will deconstruct and separate these small components to allow for recycling. For insulation, material is considered to be sent to a landfill for disposal (BIF REP, 2013). Pipework: Copper pipework follows the same EoL route as the heat exchanger from copper. Steel is recycled at a rate of 70% (Davis et al., 2006) and polyethylene EoL is split into recycling (16%), incineration (35%) and landfill (49%) (Mudgal et al., 2011) (see Supplementary Material S1 for details).

As the PP-GR composite is a relatively new material on the market, we conservatively assume landfill as the most likely fate, accounting for both polypropylene and the inert graphite.

2.4 Scenarios and functional unit

A range of scenarios has been adopted for the setup of the heat recovery system in order to represent various installation settings and compare different design options. The five scenarios are listed in Table 1. They all include the functional unit of a heat recovery system with one in-line heat exchanger, pipework of 10 m length and fittings. Separate from these scenarios, we assess the design options for the pipework, comparing copper, steel and polyethylene pipework and lengths of 1, 10 and 30 m.

Table 1: Overview of assumptions for scenarios of the LCAs.

Scenario	Name	Number of heat exchangers	Material heat exchanger	Material pipework	Length pipework
1	Copper (0%)	1	Copper (0% recycled content)	Copper (0% recycled content)	10 m
2	Copper (35%)	1	Copper (35% recycled content)	Copper (35% recycled content)	10 m
3	Copper (70%)	1	Copper (70% recycled content)	Copper (70% recycled content)	10 m
4	Copper (35%) + PE	1	Copper (35% recycled content)	Polyethylene	10 m
5	PP-GR + PE	1	Polypropylene-graphite (PP-GR)	Polyethylene	10 m

277

For the operational lifetime, we assume a conservative duration of 10 years. Other studies considered a 50-year lifetime for a copper heat exchanger or copper pipework (Asadi et al., 2016; Ip et al., 2018), but damage through corrosion is likely to occur earlier with kitchen wastewater as it carries a greater load of organic pollutants than shower drain or clean water. The functional unit for the case of an average UK kitchen is 1 kWh of water heating delivered through heat recovery.

2.5 Savings potential

In order to determine the potential environmental savings associated with use of the heat recovery system, data on recovered heat are required. We look at two different cases:

Case study: Firstly, LCA results are set into context with data on heat recovery from a case study on the restaurant kitchen of Penrhyn Castle in Bangor, North Wales, UK, which is open to visitors as a tourist attraction. Spriet and McNabola (2019b) predicted the amount of recovered heat during an 8-month monitoring study to be 8.45 kWh per day, taking into account the following: a copper heat exchanger as described above, a measured average

292 daily water consumption of 652.5 L, a 90% return rate of the consumed water into the drain, a
 293 retention time of water through kitchen appliances of no longer than 1 hour and measured
 294 average drain water temperatures of 25 to 35 °C (Supplementary Material S4). As the
 295 pipework is insulated and as time between heat recovery and consumption of the pre-heated
 296 water is very short, heat losses in the pipe are considered negligible. We consider the
 297 restaurant to be open 310 days a year. The environmental impacts realised through heat
 298 recovery are compared to the avoided impacts when replacing different conventional and
 299 renewable energy sources for water heating: natural gas, UK grid electricity, woodchips, geo
 300 and solar thermal energy, and the energy mix for water heating in the UK service sector (BEIS,
 301 2018) (Table 2; Supplementary Material S5 for environmental burdens from the energy mix).
 302 Results are presented as payback times for heat recovery when it replaces the mentioned
 303 energy sources.

304 Life cycle burdens of the heat recovery systems as in scenario 2 and 5 are considered.
 305 Scenario 2 represents the actual installations carried out at the case study site where only
 306 copper equipment was used. Scenario 5 has been selected to show potential savings with
 307 polymer-based materials.

308 *Table 2: Types of energy and respective database modules used for determination of environmental savings*
 309 *through heat recovery*

Energy type	Database module	Database	Share in UK water heating mix [%]*
Natural gas	Heat, central or small-scale, natural gas {Europe without Switzerland} market for	Ecoinvent	66
Grid electricity	Electricity, low voltage {GB} market for	Ecoinvent	14
Oil	Heat, central or small-scale, other than natural gas {Europe without Switzerland} heat production, light fuel oil, at boiler 10 kW condensing, non-modulating	Ecoinvent	12
Softwood chips	Heat, central or small-scale, other than natural gas {CH} heat production, softwood chips from forest, at furnace 50 kW, state-of-the-art 2014	Ecoinvent	4
Hardwood chips	Heat, central or small-scale, other than natural gas {CH} heat production, hardwood chips from forest, at furnace 50 kW, state-of-the-art 2014	Ecoinvent	1
Straw	Heat, district or industrial, other than natural gas {GLO} heat production, straw, at furnace 300 kW	Ecoinvent	3
Geothermal	Heat, borehole heat pump {Europe without Switzerland} heat production, borehole heat exchanger, brine-water heat pump 10 kW	Ecoinvent	n.a.
Solar thermal	Heat, central or small-scale, other than natural gas {CH} operation, solar collector system, evacuated tube collector, one-family house	Ecoinvent	n.a.

*current UK energy mix for heating water in the service sector (BEIS, 2018). The category "biomass" was split into softwood chips, hardwood chips and straw in order to best reflect the current use of biomass heat sources (BEIS 2018b, Forest Research 2018, DEFRA 2017). Neglected: bioenergy from (unless included in grid electricity): landfill gas, sewage gas, waste wood, animal biomass, anaerobic digestion and biodegradable energy from waste.

310

311 **UK commercial food outlets:** Secondly, we determine the environmental sustainability of a
 312 heat recovery system when used with typical water consumption rates prevalent in UK
 313 commercial food outlets. The water consumption rates refer to the average rates of different
 314 food outlet categories (Spriet and McNabola, 2019a), ranging from 360 to 12,500 L/day. Heat
 315 recovery data were determined as in Spriet and McNabola (2019a), (Supplementary Material
 316 S4), taking into account the number of heat exchangers optimised for maximum financial
 317 payback with 310 open days a year over a 10 year lifetime i.e. for greater flow-rates, the
 318 installation of several heat exchangers in parallel is considered (Supplementary Material S6).
 319 The life cycle burdens taken into account for the heat recovery system refer to scenario 4.

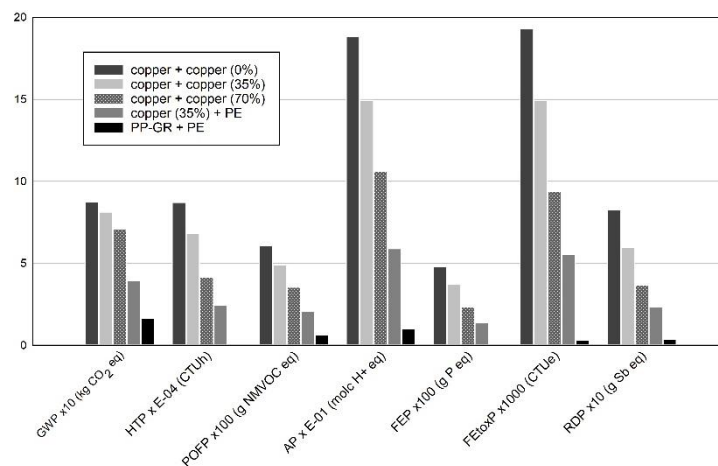
320 Finally, data on the number of served meals, water consumption and the number of outlets in
 321 the hospitality and food service sector serve to extrapolate the environmental savings to a UK
 322 level (Backman, 2018; Bromley-Challenor et al., 2013; Spriet and McNabola, 2019a).

323 3 Results and Discussion

324 3.1 Life Cycle Assessment results

325 Figure 2 shows the characterised LCA results of all scenarios for the drain water heat recovery
326 system. The different materials used for the scenarios lead to large differences between their
327 footprints. There are clear benefits from increasing the share of recycled copper or fully
328 replacing copper with polymer materials. Production, use and end-of-life of the copper systems
329 emit 87, 81 and 71 kg of CO₂ equivalent, respectively, depending on the recycled material
330 input. These numbers coincide with the findings of Giurco and Petrie (2007) who found an
331 increase in recycling rates besides demand reduction the only strategy to meet GHG reduction
332 targets for copper production as ever lower ore grades constrain the potential to decarbonise
333 copper ore processing.

334 A combination of a copper heat exchanger with polyethylene pipework has a GWP of 39 kg
335 CO₂ equivalent. Reductions in burdens of around 45-50% can be achieved for HTP, FEP,
336 FEtoXP and RDP, when switching from a heat exchanger and pipework of zero percent
337 recycled copper to one of 70% recycled copper. Replacement of the 35%-copper pipework
338 through PE can lower the impacts of the whole system by 50-60% considering the heat
339 exchanger is still made from 35%-copper. Scenario 4 therefore represents the most
340 environmentally friendly material combination currently available on the market for this set-up.



341 *Figure 2: Environmental burdens arising from the life cycle of drain water heat recovery systems consisting of in-*
342 *line heat exchanger, 10 m pipework, fittings and insulations. Percentage in brackets stands for the share of*
343 *recycled copper. PE: polyethylene, PP-GR: Polypropylene-Graphite. GWP: Global Warming Potential; HTP:*
344 *Human Toxicity Potential; POFP: Photochemical Ozone Formation Potential; AP: Acidification Potential; FEP:*
345 *Freshwater Eutrophication Potential; FEtoXP: Freshwater Ecotoxicity Potential; RDP: Mineral, fossil & renewable*
346 *Resource Depletion Potential. All scenarios as described in Table 1.*

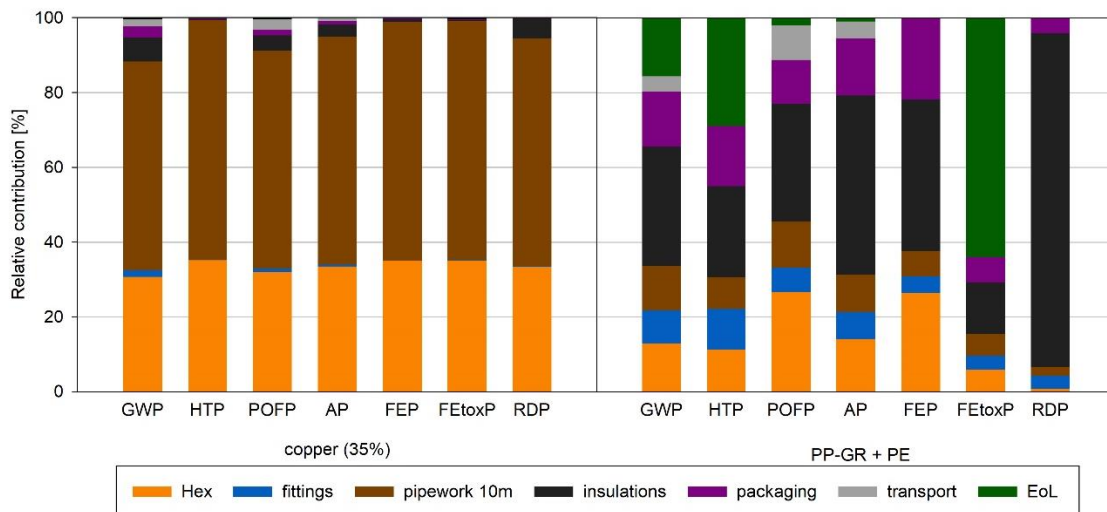
347 Still though, a purely polymer based system with PP-GR performs considerably better with a
348 GWP of only 16 kg CO₂ equivalent. Depending on the category, it exhibits only 1-20% of the
349 impacts of the 35%-copper scenario. Supplementary Material S7 shows the scenarios in a
350 relative comparison to each other. The normalised results allow for inter-category comparison
351 and show that the most relevant contributions are those to HTP and FEToxP for both systems
352 (Supplementary Material S8).

353 Ip et al. (2018) determined a GWP of 56 kg CO₂ equivalent for their copper heat exchanger,
354 which would compare to 26, 29 or 32 kg CO₂ equivalent for the life cycle of our copper heat
355 exchanger alone with 70, 35 or 0 % recycled content, respectively (excluding pipework). Their
356 study does not state the recycled copper input, making direct comparison difficult. Even so,

357 one reason for the different results is certainly the different material requirement for the heat
 358 exchanger, with about 25 kg copper in Ip's study and about 6 kg in this study.

359 Figure 3 shows the relative contribution of the life cycle stages to the environmental burdens
 360 of heat recovery systems under scenario 2 and 5. The majority of burdens of the copper
 361 system across all categories originate from manufacture of copper parts (heat exchanger and
 362 pipework), ranging from 87% of GWP burdens to 99% of HTP, FEP and FEtoXP burdens. This
 363 underlines the pollution associated with the extraction and manufacture of copper products
 364 discussed earlier in the introduction (Althaus and Classen, 2005; Castro Molinare, 2014).
 365 Indeed, the main burdens from the manufacture of heat exchanger and pipes derive from the
 366 generation of primary copper (Ecoinvent, 2018): HTP causing emissions arise mainly during
 367 the treatment of sulfidic tailings from primary copper production and comprise groundwater
 368 polluting zinc and arsenic (HTP non-cancer), and chromium VI (HTP cancer), amongst others.
 369 Similarly, FEToxP is mainly caused by zinc and copper emissions from tailing treatment and
 370 FEP predominantly through phosphate released into groundwater during the same process
 371 (Ecoinvent, 2018). The main substances responsible for POFP are nitrogen oxides emitted
 372 into the air during blasting, which also releases sulphur dioxide, the major cause for AP.
 373 Resource depletion is caused especially by use of the sulfidic copper ore and molybdenum
 374 during primary copper generation. Other resources contribute less than 1% to the RDP, hence
 375 RDP is almost exclusively due to the consumption of abiotic materials. Only for GWP, the
 376 finishing process of the heat exchanger and pipes has a greater influence than primary copper
 377 production driven by heat and electricity consumption. The impact from the pipework is greater
 378 than that from the heat exchanger, which is due to greater material use for the 10 m pipework
 379 (11 kg vs. 6 kg copper).

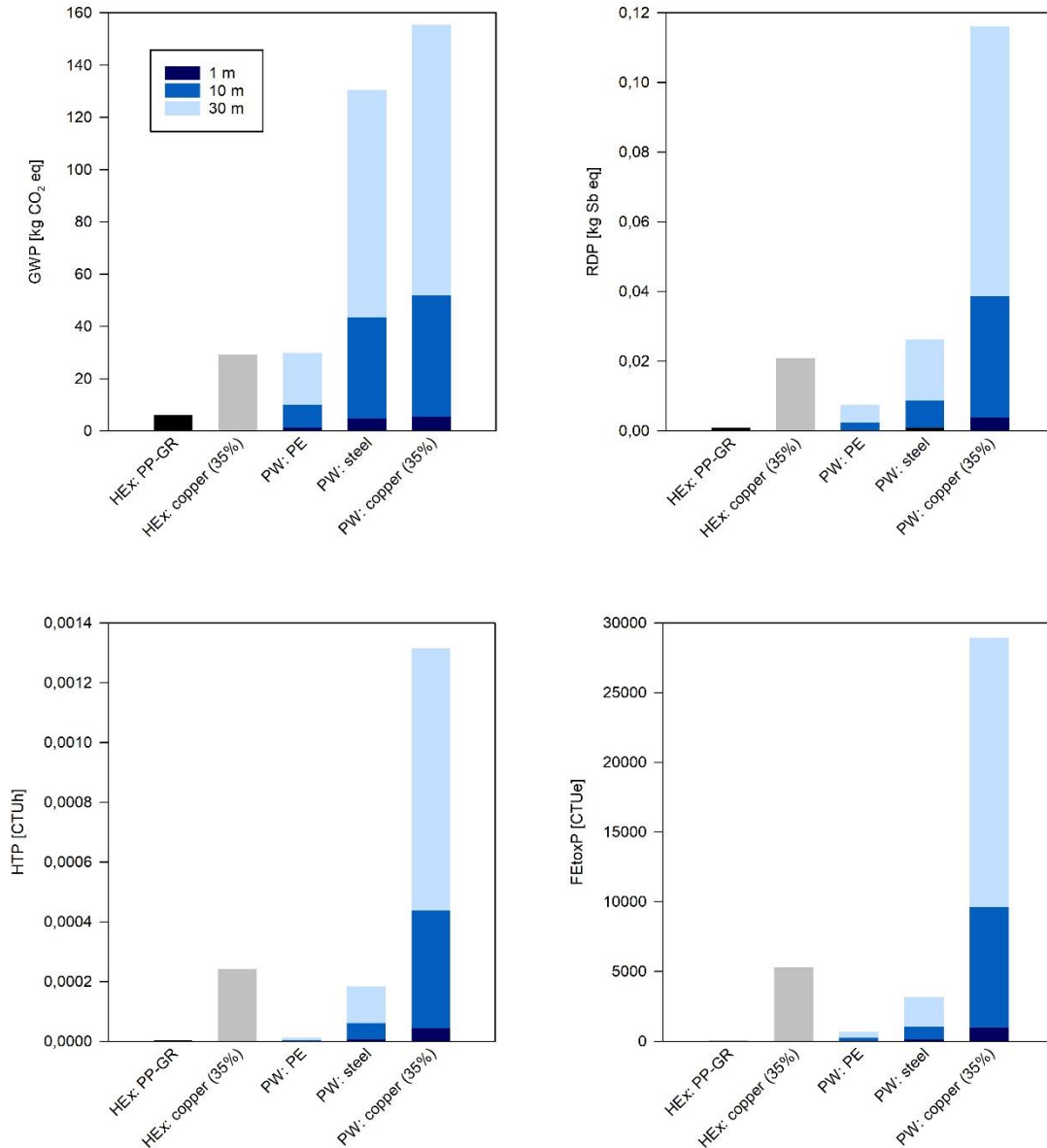
380 In the PP-GR system, the manufacture of the heat exchanger and pipework plays a
 381 comparatively smaller role. Apart from transport, all components make significant
 382 contributions to the lower overall impacts, depending on the category. Manufacture of the
 383 insulation from EPDM rubber accounts for 14-90% of burdens, with the greatest contribution
 384 going to RDP. The main resource depleted is indium during the operation of the zinc mine,
 385 zinc being an ingredient for the production of EPDM (Ecoinvent, 2018). EoL stage is mainly
 386 responsible for impacts in FEToxP (64%), HTP (29%) and GWP (16%). FEToxP causing
 387 emissions in the EoL stage are arising from incineration and landfilling of the pipe material PE,
 388 both processes releasing vanadium into groundwater (Ecoinvent, 2018). The contribution of
 389 the predominantly cardboard packaging ranges from 4% (RDP) to 22% (FEP) across
 390 categories.



391

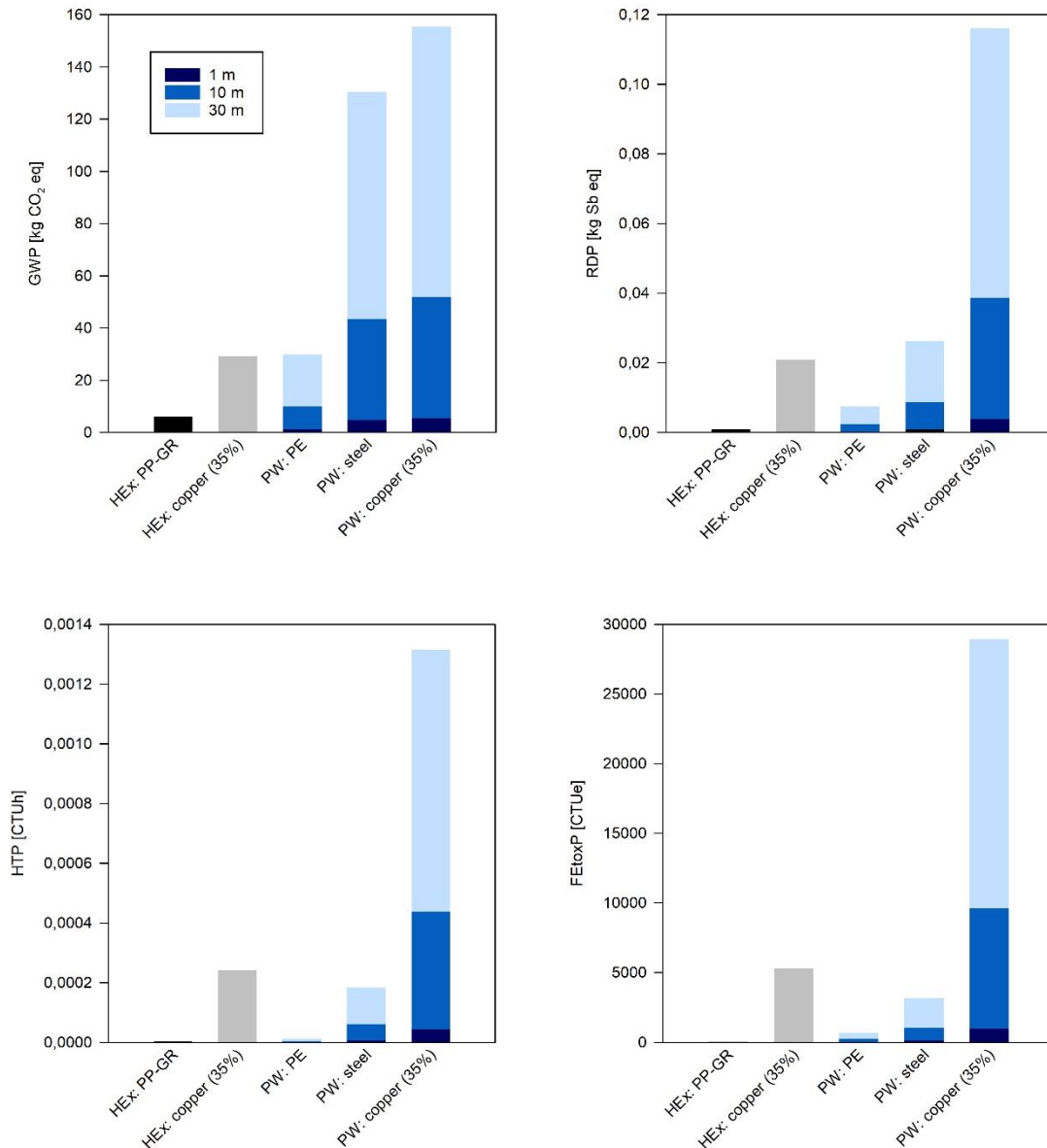
392 Figure 3: LCA of heat recovery systems (scenarios 2 and 5): Relative contribution of the life cycle stages to the
 393 environmental impacts of the two heat recovery systems including 10 m pipework. Left: scenario 2: copper
 394 system with 35% recycled copper input. Right: scenario 5: PP-GR composite system with PP-GR heat exchanger
 395 and pipework from PE. GWP: Global Warming Potential; HTP: Human Toxicity Potential; POFP: Photochemical
 396 Ozone Formation Potential; AP: Acidification Potential; FEP: Freshwater Eutrophication Potential; FEToxP:
 397 Freshwater Ecotoxicity Potential; RDP: Mineral, fossil & renewable Resource Depletion Potential; Hex: Heat
 398 exchanger; EoL: End of Life.

399 The length of the pipework greatly influences the overall LCA results.



400

401 Figure 4 shows the burdens from heat exchanger and pipework separately. Burdens for long
 402 and metal based (steel or copper) pipework can be greater than those from the heat
 403 exchanger. Steel pipe burdens are considerably lower than copper pipe burdens, ranging from
 404 89% (FEToxP) to 15% (GWP) of those from copper (see Supplementary Material S9 for more
 405 impact categories). These results underline the importance of considering the full equipment
 406 necessary for retrofit, and also how on-site conditions influence the environmental
 407 sustainability of a retrofit measure. As far as we are aware, this is the first LCA study of a heat
 408 recovery system to consider all associated retrofit pipework.



409

410 *Figure 4: Comparison of LCA results for the heat exchanger and pipework for (clockwise from top left): global*
 411 *warming potential (GWP), resource depletion potential (RDP), freshwater ecotoxicity potential (FEtoXP) and*
 412 *human toxicity potential (HTP). Left two bars: complete life cycle of a heat exchanger system without pipework.*
 413 *Right three bars: life cycle of pipework from polyethylene (PE), steel and copper (35% recycled content).*

414 3.2 Environmental savings through heat recovery

415 3.2.1 Environmental savings in the case study

416 In the Penrhyn Castle case study, all environmental burdens from the heat recovery system
 417 (scenario 2) will be paid back within 10 years when electricity, geo or solar thermal energy or
 418 the energy mix for water heating is replaced (Table 3). If the recovered heat replaces natural
 419 gas, the impacts of HTP, FEP, FEtoXP and RDP from production, installation and EoL of the
 420 heat exchanger and pipework will not be fully paid back in the conservative 10-year lifetime
 421 considered in this study. The low FEtoXP and RDP of wood heating also prevent payback in
 422 the FEtoXP and RDP categories through heat recovery if wood is used for water heating. For
 423 GWP, relatively short payback times of under 1.6 years compared with all energy alternatives
 424 can be achieved. The payback time for GWP compared to natural gas, the most common

425 water heating source, is only 0.12 years. This is shorter than the 0.55-1.33 year GWP payback
 426 previously calculated for shower heat recovery (Ip et al., 2018). It underpins the suitability of
 427 kitchens for drain water heat recovery due to typically higher wastewater flow-rates than in
 428 showers.

429 As the burdens of the PP-GR heat recovery system are substantially lower, they are paid back
 430 during shorter periods of operation, within 2 years for all impact categories (Table 3).

431 *Table 3: Environmental payback times in years for the heat recovery system of the Penrhyn Castle case study.*
 432 *Comparison of the copper (35% recycled content) and the PP-GR systems including 10 m of pipework with*
 433 *different energy sources for water heating. Bold and italic: Impacts are not paid back within a 10-year lifetime. NG*
 434 *= natural gas. Mix: Current UK Energy mix for heating water in the service sector (BEIS, 2018). GWP: Global*
 435 *Warming Potential; HTP: Human Toxicity Potential; POFP: Photochemical Ozone Formation Potential; AP:*
 436 *Acidification Potential; FEP: Freshwater Eutrophication Potential; FEToxP: Freshwater Ecotoxicity Potential;*
 437 *RDP: Mineral, fossil & renewable Resource Depletion Potential. Energy sources as in Table 2.*

Impact category	NG	Electricity	Wood	Geo	Solar	Mix
Copper (35%)	[years]					
GWP	0.12	0.06	0.29	0.23	1.58	0.11
HTP	18.87	1.22	2.13	3.76	3.20	5.04
POFP	0.72	0.13	0.27	0.61	2.05	0.40
AP	1.82	0.16	1.19	0.60	1.90	0.68
FEP	12.20	0.59	8.79	1.10	3.31	3.19
FEToxP	14.16	0.52	11.78	1.72	3.51	3.02
RDP	14.32	2.94	33.49	8.41	3.63	9.23
PP-GR + PE	[years]					
GWP	0.02	0.01	0.05	0.04	0.27	0.02
HTP	0.16	0.01	0.02	0.03	0.03	0.04
POFP	0.08	0.01	0.03	0.07	0.23	0.04
AP	0.10	0.01	0.07	0.03	0.11	0.04
FEP	0.19	0.01	0.13	0.02	0.05	0.05
FEToxP	0.25	0.01	0.21	0.03	0.06	0.05
RDP	0.73	0.15	1.71	0.43	0.19	0.47

438

439

440 **3.2.2 Environmental savings in UK commercial food outlets**

441 Two different flow-rates, representing the bottom and top end of the flow-rate spectrum in
 442 typical UK food outlets, are taken to show a worst- and best-case scenario for environmental
 443 impacts from heat recovery. The best case refers to kitchens with the highest water flow-rate
 444 typically found in UK food outlets (12,500 L/day), highest heat recovery potential and therefore
 445 the lowest impacts per kWh (“H recov. Low”). The opposite applies to the worst-case scenario
 446 with a flow-rate of 360 L/day (“H recov. High”). The environmental burdens for the heat
 447 recovery system are based on scenario 4 (Table 1), including one heat exchanger for the low-
 448 flow option and four heat exchangers in parallel for the high-flow option.

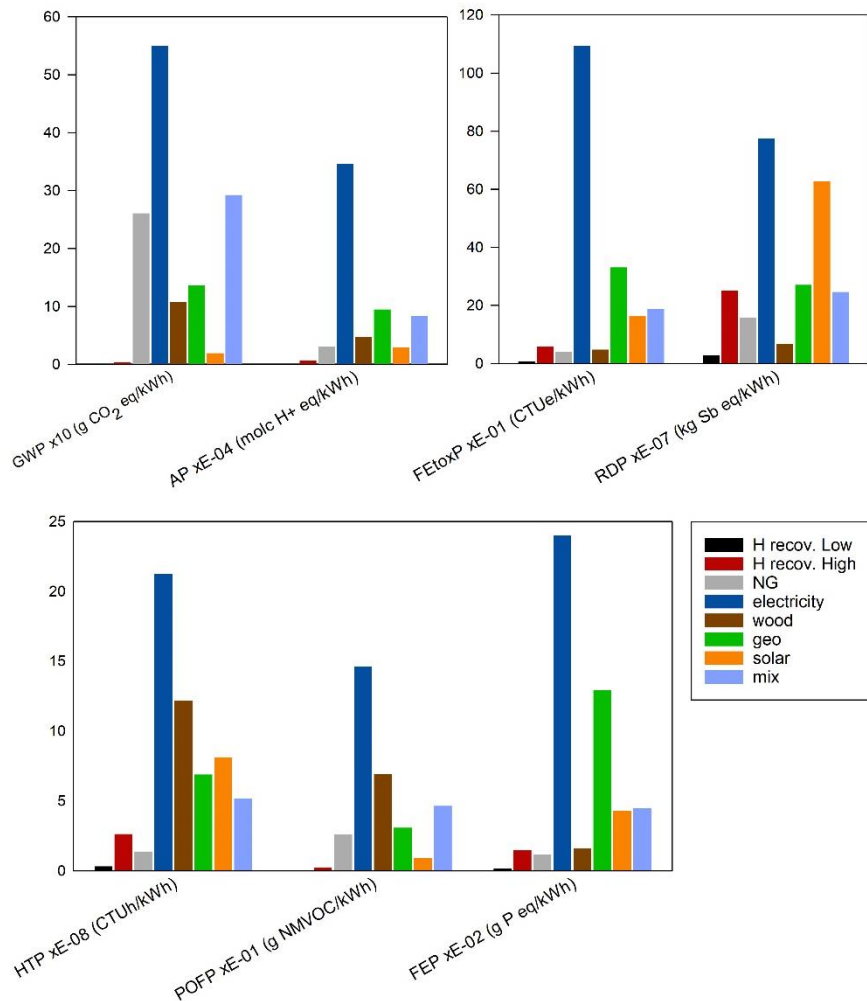
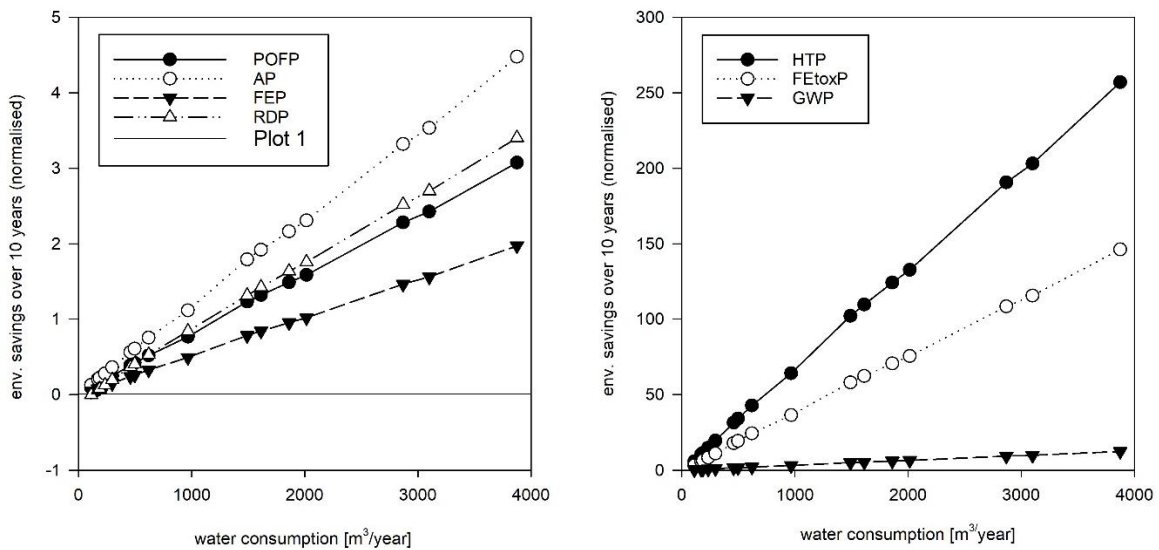


Figure 5: Environmental impacts per kWh for water heating. Comparison of heat recovery from drain water with other renewable and non-renewable heat sources, including the current UK energy mix for water heating (“mix”). Burdens of the heat recovery system as in scenario 4 with two different water flow-rates found in UK commercial food outlets. H recov. Low: low impact case due to higher flow-rate of 12,500 L/day. H recov. High: high impact case due to lower flowrate of 360 L/day. NG: natural gas, electricity: UK grid mix, wood: wood biomass combustion, geo: geothermal, solar: solar thermal. GWP: Global Warming Potential; HTP: Human Toxicity Potential; POFP: Photochemical Ozone Formation Potential; AP: Acidification Potential; FEP: Freshwater Eutrophication Potential; FEtoXP: Freshwater Ecotoxicity Potential; RDP: Mineral, fossil & renewable Resource Depletion Potential.

449 Figure 5 displays the environmental impacts for providing 1 kWh for water heating through
 450 heat recovery versus other energy sources. Considering global warming, heating water
 451 through the use of recovered heat exhibits the lowest emissions with about 0.4 to
 452 4 g CO₂ equivalent/kWh for the low and high impact scenario, respectively. This compares to

453 emissions of 20 to 550 g CO₂ equivalent/kWh for solar thermal and electric water heating –
 454 i.e. even when currently available heat recovery technology replaces renewable energy
 455 sources, GWP can be reduced. Also for ozone formation and acidification, heat recovery at
 456 both flow-rates leads to impact savings compared to all other heat sources. In the other
 457 categories, environmental sustainability of heat recovery depends on the flow-rate or the
 458 heating source replaced. For HTP and FEP, natural gas water heating can have lower
 459 environmental impacts compared to heat recovery at low flow-rates. Here, emission savings
 460 through heat recovery are only achieved from a flow-rate of about 750 L/day onwards (HTP)
 461 and 555 L/day (FEP) (values not shown in graph). Similarly, FEtoX and RDP can be reduced
 462 through heat recovery at higher flow-rates only, when replacing natural gas or wood biomass.
 463 With these results a recommendation for drain water heat recovery can be given from a daily
 464 flow-rate of 750 L when natural gas is replaced, the most common source for water heating in
 465 the UK.

466 Figure 6 shows the environmental savings that can be achieved during 10 years of heat
 467 recovery depending on the flow-rate and replacing the water heating energy mix. Values are
 468 shown as normalised scores. The net environmental savings increase with water
 469 consumption, although the number of heat exchangers and with them the environmental
 470 footprint of the installations augments, too. Apart from RDP, environmental payback is reached
 471 within 10 years for all impact categories starting from the lowest average daily water
 472 consumption considered (360 L/day) (Spriet and McNabola, 2019a). For RDP, environmental
 473 payback within 10 years is only achieved at water consumption rates above approximately
 474 555 L/day or 300 m³/year. The greatest normalised savings are achieved in HTP and FEtoX P,
 475 followed by GWP, AP, RDP, POFP and FEP in descending order.



476

477 *Figure 6: Normalised net environmental savings (positive values) through heat recovery from a commercial*
 478 *kitchen after 10 years depending on the yearly water consumption. GWP: Global Warming Potential; HTP:*
 479 *Human Toxicity Potential; POFP: Photochemical Ozone Formation Potential; AP: Acidification Potential; FEP:*
 480 *Freshwater Eutrophication Potential; FEtoXP: Freshwater Ecotoxicity Potential; RDP: Mineral, fossil & renewable*
 481 *Resource Depletion Potential.*

482 Extrapolation of the savings using average daily water consumption rates for the about
 483 258,000 food outlets in the UK (in 2017) (Backman, 2018; Bromley-Challenor et al., 2013;
 484 Spriet and McNabola, 2019a) gives the potential of environmental savings for the UK per year
 485 (Table 4). Annual GHG emission mitigation of 490 Gg (kilo-tonnes) CO₂ equivalent could be

486 avoided if heat from wastewater was recovered across all UK commercial food outlets. These
 487 environmental savings relate to heat savings of 30% compared to the thermal energy needed
 488 for water heating in the hospitality and food service sector, estimated with the share of hot
 489 water consumed in the Penrhyn Castle restaurant.

490 The results show that even with the currently available copper heat exchanger and especially
 491 at high water consumption rates, there is strong evidence for environmental savings. It can
 492 therefore be recommended as a viable measure to de-carbonise water heating in commercial
 493 kitchens.

494 *Table 4: Yearly net environmental savings potential for the UK through heat recovery from wastewater in all*
 495 *commercial food outlets. eq = equivalent*

Impact category	GWP	HTP	POFP	AP	FEP	FEtoXP	RDP
Unit	[kt CO ₂ eq]	[CTUh]	[t NMVOC eq]	[1000 molc H+ eq]	[t P eq]	[10 ⁶ CTUe]	[kg Sb eq]
All outlets	490	78	772	1390	70	2979	3370

496

497 Although an economic evaluation of the heat recovery system is out of scope of this study, it
 498 is worth mentioning that heat recovery is not only beneficial from an environmental point of
 499 view, but also pays back financially from water consumption rates of 960 L/day (Spriet and
 500 McNabola, 2019a).

501 A study by McNabola and Shields (2013) estimated the heat recovery potential from shower
 502 drain water in Ireland to be 808 GWh per year, averaging 577 kWh per year for a 3-person
 503 household. Taking into account the population of the UK of 66M (ONS, 2019) and the UK
 504 domestic energy mix for water heating (BEIS, 2018), this would translate to yearly savings of
 505 13 TWh or 3600 Gg CO₂ equivalent. Based on the heat recovery system evaluated in this
 506 study, the aforementioned annual heat recovery at a household scale would not be financially
 507 viable, nor environmentally responsible from a resource depletion perspective.

508 3.3 Outlook

509 3.3.1 Expected changes with a changing energy mix

510 With a change in the future energy mix towards more renewable sources, the benefit of saving
 511 energy through heat recovery is likely to shift from avoiding GHG emissions, to avoiding the
 512 depletion of metal and mineral resources. GHG emission savings through heat recovery will
 513 be lower as water heating from renewable energy sources emits less GHGs, for both direct
 514 electric water heating and thermal water heating with solar collectors or air and ground-source
 515 heat pumps (Clarke et al., 2008). Although of course, the GHG emissions of producing the
 516 heat recovery system and pipework are also expected to decrease owing to decarbonisation
 517 of energy supplies.

518 Resource depletion burdens are higher for renewable electricity generation (namely wind,
 519 solar and hydro power) compared to energy supply from fossil resources owing to large
 520 quantities of abiotic resources, especially metals (e.g. manganese, copper, iron, nickel,
 521 chrome) required in renewable energy infrastructure (Berrill et al., 2016; Gallagher et al.,
 522 2019). The trade-offs between resource depletion and GHG emission savings which currently
 523 exist for heat recovery at low flow-rates are therefore likely to disappear.

524 Another important indirect and long-term benefit of heat recovery lies in increasing the
 525 efficiency in which energy is used and thus supporting a transformation to a sustainable
 526 energy economy through reducing energy demand – a strategy that has been adopted as part

527 of European and UK policies for future low-carbon energy supply (Clarke et al., 2008; da Graça
528 Carvalho, 2012; Ekins and Lees, 2008; Rosenow, 2012).

529 **3.3.2 Recommendation for further research**

530 As neither the copper nor the PP-GR heat exchanger have been in use with kitchen drain
531 water for significant periods of time, there is room for further research and need for empirical
532 data on real performance. In addition to environmental savings during manufacture, PP-GR
533 and similar composites can offer other potential advantages such as the reduction of scaling
534 in the pipe and thus reduced build-up of an insulating layer inhibiting heat transfer. The
535 behaviour of new materials for this application, but also the behaviour of the conventional
536 copper heat exchanger when used with heavily polluted wastewater such as that from
537 kitchens, requires long-term experimental studies. This will provide more reliable data on heat
538 transfer performance and on required maintenance interventions such as cleaning to remove
539 scaling or fouling. It will also allow more accurate determination of the useful lifetime of the
540 heat exchangers, which will be important for both economic and environmental performance.
541 The lack of accurate data sets and reliance on manufacturer data for modelling the PP-GR
542 material are aspects which should improve with increasing use of such materials.

543 **4 Conclusions**

544 The presented LCA study is the first to evaluate the environmental sustainability of a heat
545 recovery system for harvesting the heat of commercial kitchens' drain water, based on case
546 study data. Different sets of materials are studied for the system, comparing components from
547 conventional copper with alternatives from polypropylene and graphite, as well as
548 polyethylene. The results support the following conclusions:

- 549 • The environmental impacts from the copper system, predominantly arising from the
550 production of primary copper, can be reduced substantially through increasing the
551 share of recycled copper as input material.
- 552 • A critical factor influencing the material requirement and environmental footprint of any
553 retrofitted (or new) heat recovery system is the length of pipework necessary for
554 connecting the heat exchanger with boiler and cold water supply. We therefore
555 recommend to design the system as compact as possible.
- 556 • It is strongly encouraged to consider material choice during the design phase of such
557 installations, including the use of recycled material or new functional materials, such
558 as the polypropylene-graphite composite.
- 559 • Heat recovery shows environmental trade-offs with other water heating sources only
560 for flowrates at the lower end of the spectrum of typical water consumption rates in UK
561 food outlets, mainly for resource depletion.
- 562 • The amount of recovered heat and with it the environmental savings increase with the
563 water consumption rate, even when environmental capital costs are increased through
564 the installation of several heat exchangers in parallel. Environmental savings across
565 all seven impact categories analysed is achieved for water consumption above
566 555 L/day when replacing the heating energy mix.
- 567 • Heat recovery from wastewater from food outlets offer a potential solution for saving
568 energy and emissions across the food service sector. When applied across all UK food
569 outlets, GHG emission savings can amount 490 Gg CO₂ equivalent per year.

570
571

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576

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747 **Figure and Table Captions:**

748 *Figure 7: System boundaries of the LCAs on the heat recovery system (left, shown for the copper system) and*
749 *extended boundaries for evaluating the savings potential through the replacement of heat energy sources.*

750 *Figure 2: Environmental burdens arising from the life cycle of drain water heat recovery systems consisting of in-*
751 *line heat exchanger, 10 m pipework, fittings and insulations. Percentage in brackets stands for the share of*
752 *recycled copper. PE: polyethylene, PP-GR: Polypropylene-Graphite. GWP: Global Warming Potential; HTP:*
753 *Human Toxicity Potential; POFP: Photochemical Ozone Formation Potential; AP: Acidification Potential; FEP:*
754 *Freshwater Eutrophication Potential; FEToxP: Freshwater Ecotoxicity Potential; RDP: Mineral, fossil & renewable*
755 *Resource Depletion Potential. All scenarios as described in Table 1.*

756 *Figure 3: LCA of heat recovery systems (scenarios 2 and 5): Relative contribution of the life cycle stages to the*
757 *environmental impacts of the two heat recovery systems including 10 m pipework. Left: scenario 2: copper system*
758 *with 35% recycled copper input. Right: scenario 5: PP-GR composite system with PP-GR heat exchanger and*
759 *pipework from PE. GWP: Global Warming Potential; HTP: Human Toxicity Potential; POFP: Photochemical Ozone*
760 *Formation Potential; AP: Acidification Potential; FEP: Freshwater Eutrophication Potential; FEToxP: Freshwater*
761 *Ecotoxicity Potential; RDP: Mineral, fossil & renewable Resource Depletion Potential; Hex: Heat exchanger; EoL:*
762 *End of Life.*

763 *Figure 4: Comparison of LCA results for the heat exchanger and pipework for (clockwise from top left): global*
764 *warming potential (GWP), resource depletion potential (RDP), freshwater ecotoxicity potential (FEToxP) and*
765 *human toxicity potential (HTP). Left two bars: complete life cycle of a heat exchanger system without pipework.*
766 *Right three bars: life cycle of pipework from polyethylene (PE), steel and copper (35% recycled content).*

767 *Figure 8: Environmental impacts per kWh for water heating. Comparison of heat recovery from drain water with*
768 *other renewable and non-renewable heat sources, including the current UK energy mix for water heating (“mix”).*
769 *Burdens of the heat recovery system as in scenario 4 with two different water flow-rates found in UK commercial*
770 *food outlets. H recov. Low: low impact case due to higher flow-rate of 12,500 L/day. H recov. High: high impact*
771 *case due to lower flowrate of 360 L/day. NG: natural gas, electricity: UK grid mix, wood: wood biomass*
772 *combustion, geo: geothermal, solar: solar thermal. GWP: Global Warming Potential; HTP: Human Toxicity*
773 *Potential; POFP: Photochemical Ozone Formation Potential; AP: Acidification Potential; FEP: Freshwater*
774 *Eutrophication Potential; FEToxP: Freshwater Ecotoxicity Potential; RDP: Mineral, fossil & renewable Resource*
775 *Depletion Potential*

776 *Figure 6: Normalised net environmental savings (positive values) through heat recovery from a commercial kitchen*
777 *after 10 years depending on the yearly water consumption. GWP: Global Warming Potential; HTP: Human Toxicity*
778 *Potential; POFP: Photochemical Ozone Formation Potential; AP: Acidification Potential; FEP: Freshwater*
779 *Eutrophication Potential; FEToxP: Freshwater Ecotoxicity Potential; RDP: Mineral, fossil & renewable Resource*
780 *Depletion Potential.*

781 *Table 1: Overview of assumptions for scenarios of the LCAs.*

782 *Table 2: Types of energy and respective database modules used for determination of environmental savings*
783 *through heat recovery*

784 *Table 3: Environmental payback times in years for the heat recovery system of the Penrhyn Castle case study.*
785 *Comparison of the copper (35% recycled content) and the PP-GR systems including 10 m of pipework with different*
786 *energy sources for water heating. Bold and italic: Impacts are not paid back within a 10-year lifetime. NG = natural*
787 *gas. Mix: Current UK Energy mix for heating water in the service sector (BEIS, 2018). GWP: Global Warming*
788 *Potential; HTP: Human Toxicity Potential; POFP: Photochemical Ozone Formation Potential; AP: Acidification*
789 *Potential; FEP: Freshwater Eutrophication Potential; FEToxP: Freshwater Ecotoxicity Potential; RDP: Mineral,*
790 *fossil & renewable Resource Depletion Potential. Energy sources as in Table 2.*

791 *Table 4: Yearly net environmental savings potential for the UK through heat recovery from wastewater in all*
792 *commercial food outlets. eq = equivalent*